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# Crystallization Kinetics and Magnetic Properties of $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$ Amorphous Ribban

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**Abstract** Fe-based bulk metallic glasses (BMGs) have been extensively studied due to their potential technological applications and their interesting physical and mechanical properties such as a low modulus of elasticity, high yielding stress and good magnetic properties. In the present work, the amorphous ribbon formation of  $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$  (numbers indicate at. %) with a ribbon form was fabricated by the single roller melt-spinning method. Rapid solidification leads to a fully amorphous structure for all compositions. The thermal properties associated with crystallization temperature of the glassy samples were measured using differential scanning calorimetry (DSC) at a heating rate of  $10^\circ\text{C}/\text{mn}$ . The microstructure and phase formation of the alloy have been analyzed by using X-ray diffractometry (XRD). The effect of high temperature on the isothermal crystallization of  $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$  ribbon was investigated by HTX-ray diffraction. In addition, these ribbon glasses also exhibit good soft magnetic properties with M-H curvature were measured under the magnetic fields between  $-1$  kOe and  $1$  kOe.

**Keywords** Bulk Metallic Glasses, Amorphous Ribbon, DSC, HTXRD Method, Magnetic Properties

## 1. Introduction

Magnetic materials have undoubtedly played a central role in the process of rapid technological innovation and evolution. However, there are still limitations, related to non-optimal properties and use of electro-magnetic materials in various devices and appliances. In particular, in the last decades the electrical utility industry has dramatically increased the monetary value placed on transformer losses as part of an overall effort to increase electric power generation and distribution efficiency. To meet this challenge, transformers manufacturers have

introduced new transformer designs and have investigated new transformer core materials aimed at reducing core losses to replace silicon steel. To this aim, metallic glasses, because of their low core loss have received considerable attention for use as a core material in high frequency transformers [1]. These have been observed to have unique electronic and mechanical properties arising from a lack of long-range crystallographic order. High cooling rates (above  $105$  K/s) are required for glass formation to produce amorphous alloys leading to samples in the form of thin sheets with thickness limited to hundreds of  $\mu\text{m}$ . Among these systems a great role has been played by the ferromagnetic Fe-, Co- and Ni-based amorphous presently widely exploited in core transformers [2].

The major reason for the low-core losses of these systems can be basically ascribed to large electrical resistivity and low magnetic coercivity. However, the quest for advanced engineering materials having simultaneously high glass forming ability, super high strength and excellent magnetic properties is always very stringent due to the need of saving energy.

After the discovery that multi component alloys could be cast from the liquid state in a fully amorphous state at cooling rate of  $\approx 10$  K/s has stimulated intensive research due to perspective applications [3]. In particular, magnetic bulk metallic glasses (BMG) have been widely investigated despite the non-excellent magnetic properties, due to the possibility of directly casting the materials with different shapes having predefined dimensions. The first room temperature ferromagnetic BMG have been synthesized in 1993. In 1995, Inoue et al. produced Fe-based bulk magnetic systems displaying soft magnetic properties containing a very large number of elements [4]. Since then a variety of Fe, Zr, Co, and Ni-based bulk glassy alloys have been produced [5, 6].

The present study has been carried out to synthesize a ribbon amorphous  $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$  alloy with of  $5$  mm width and about  $30$   $\mu\text{m}$  thickness was prepared using a single-roller,

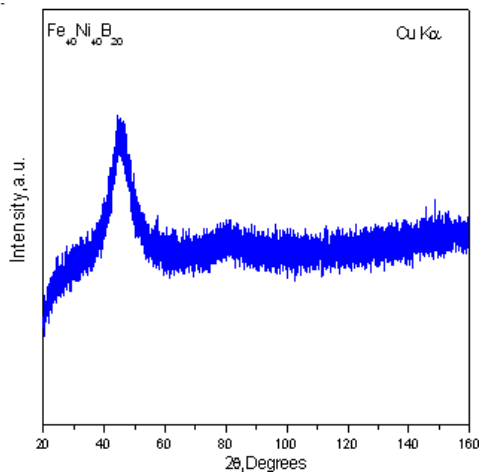
melt spinning technique under a vacuum atmosphere. The stability of the glassy matrix and the crystallization (formed phases, kinetic...) have been studied by different methods (DSC, HTX-ray diffraction). The magnetic properties of Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> are measured at room temperature.

## 2. Experimental

An ingot of the Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> alloy (composition is given in nominal atomic percentages) was prepared by arc-melting mixtures of Fe 99.99 mass% purity, Ni 99.8 mass% purity and B 99.9 mass% purity in an argon atmosphere purified using Ti-gettering. From the master alloy ingot, a ribbon of 5 mm width and about 30 μm thickness was prepared using a single-roller, melt spinning technique under a vacuum atmosphere. The structure of the samples was examined by X-ray diffraction (XRD) with Cu Kα ( $\lambda = 1.54056 \text{ \AA}$ ) radiation. The thermal stability associated with the glass transition, super cooled liquid region and crystallization of the glassy alloys was investigated by differential scanning calorimetry (DSC) at a heating rate of 10°C/mn. The hysteresis loops of the alloys with different Hf contents were recorded with a superconducting quantum interference device (SQUID) under an applied magnetic field of maximum 1 kOe at room temperature.

## 3. Results and Discussion

Fig. 1 shows the X-ray diffraction pattern for the melt-spun ribbon Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> alloy. The pattern consists of a broad diffused maximum without diffraction peaks corresponding to crystalline phases. Consequently, the formation of a single glassy phase for the Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> alloy is confirmed.

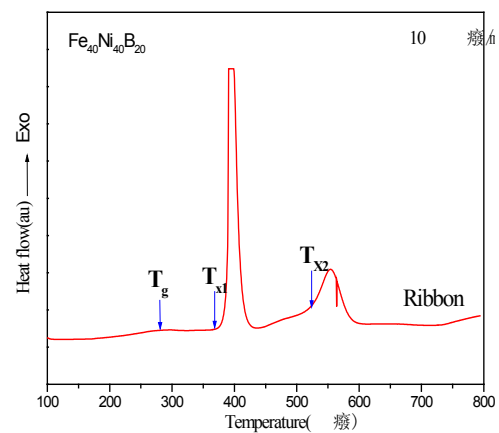


**Figure 1.** X-ray diffraction pattern on the melt-spun amorphous ribbon Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> alloy

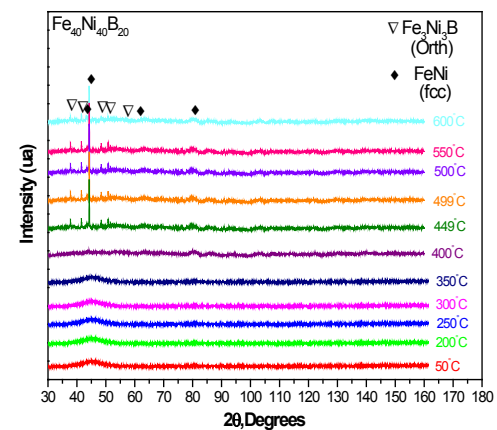
The critical cooling rate for glass formation,  $R_c$ , is an important characteristic parameter for predicting the ease or difficulty of glass formability. It is defined as the minimum

cooling rate necessary to keep the melt amorphous without detectable crystallization upon solidification. A slower  $R_c$  indicates a greater glass-forming ability of an alloy system.

Fig. 2 shows the DSC trace for the ribbon Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> metallic glass obtained at the constant heating rate of 10°C/mn. As shown in Fig. 2, a distinct endothermic reaction associated with glass transition can be observed over the temperature  $T_g$  is 281°C. At temperatures above glass transition, the alloy exhibits a wide super cooled liquid region defined as the temperature interval  $\Delta T_x = T_{x1} - T_g = 105^\circ\text{C}$ , where  $T_{x1}$  is the onset temperature of crystallization,  $T_g$  the temperature of glass transition. This indicates that the Fe-based ribbon glassy alloy has a high thermal stability, which allows the mechanical spectroscopy measurement to be performed in deeply super cooled liquid region. For Fe based alloy, two crystallization events are visible following the super cooled liquid region: The first one is characterized by a sharp and large exothermic peak, associated with the crystallization of the amorphous matrix. In contrast, the second is a relatively smaller one, which may be induced by the secondary crystallization of the remaining super cooled liquid or the transformation of the primary metastable phase



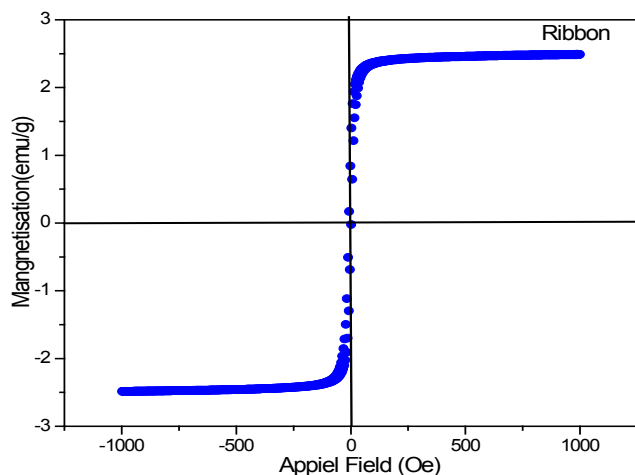
**Figure 2.** DSC curves of Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> amorphous ribbon



**Figure 3.** HTXRD scans of in situ annealed sample of Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> amorphous ribbon

The structural evolution during heating was investigated

by XRD. The diffraction patterns of melt-spun ribbon heated to different temperatures are shown in Fig. 7, together with the pattern of the as-prepared sample. The ribbon broad maxima characteristic for amorphous materials and no trace of crystalline phases, indicating that they are in the amorphous state for temperatures between 200°C and 350°C. The phase formation reflects at the ( $T=400^\circ\text{C}$ ). Obviously, the first step of devitrification is mostly linked with the formation of quasicrystalline phase, as other crystalline phase (orthogonal  $\text{Fe}_3\text{Ni}_3\text{B}$ ,  $\text{FeNi}$ ) only exist in between 449°C and 600°C.



**Figure 4.** Magnetization curves ( $M$ - $H$  loops) of  $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$  amorphous ribbon measured at room temperature

The hysteresis  $M$ - $H$  loops  $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$  alloy ribbon is illustrated in Fig. 4. Magnetization rises sharply with increasing field under the lower field side and becomes saturated under the higher applied field for  $\text{Fe}_{40}\text{Ni}_{40}\text{B}_{20}$  amorphous ribbon, which is the evidence of ferromagnetism. The saturation magnetization is 2.5 emu/g at room temperature, and displays typical features of a soft magnetic material.

## 4. Conclusions

The stable crystalline phases include cubic orthogonal  $\text{Fe}_3\text{Ni}_3\text{B}$  and fcc  $\text{FeNi}$  after complete crystallization of ribbon only exist in between 449°C and 600°C. In addition, the amorphous ribbon also shows soft magnetic material

which would be a promising candidate to replace the Fe-Si alloy in transformer cores should possess higher magnetization at saturation of 2.5 emu/g, higher permeability, higher electrical resistivity, higher Curie temperature and lower loss in dynamic magnetization process than the current commercially produced silicon steels. That will be performed in the near future.

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